

# CHARACTERIZATION OF THE BI-PHASE CO<sub>2</sub> COOLING SYSTEM MARTA FOR QUALITY CONTROL IN THE ITK PIXEL DETECTOR PRODUCTION

Bachelorcolloquium presented by Dominik Hauner,  
examined by  
Prof. Dr. Klaus Desch and Dr. Matthias Hamer  
24.10.2023



## OUTLINE

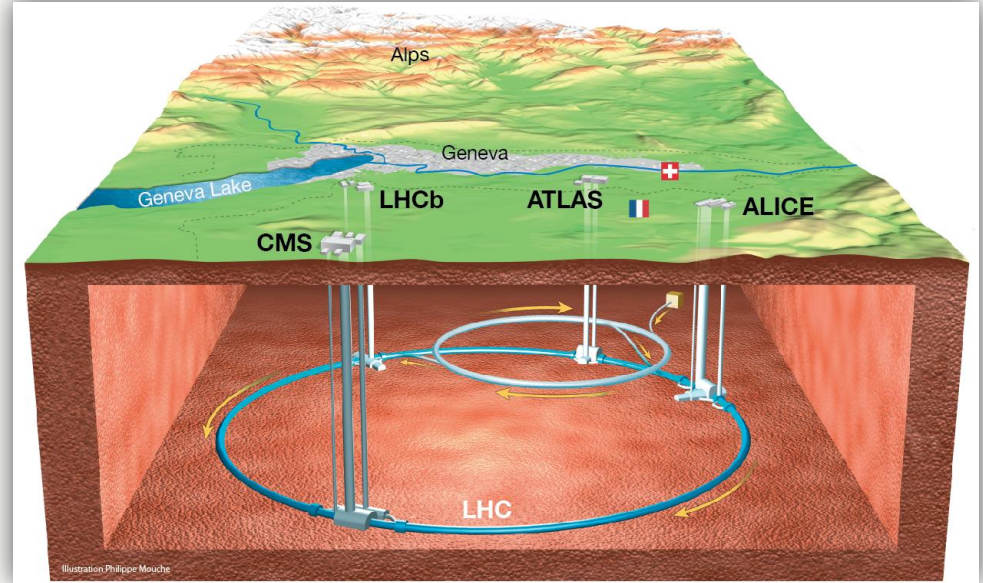
1. The ITk pixel detector
2. Cooling systems
- 3. Characterization of MARTA**
4. Summary and outlook



# The ITk pixel detector

# HIGH LUMINOSITY LHC

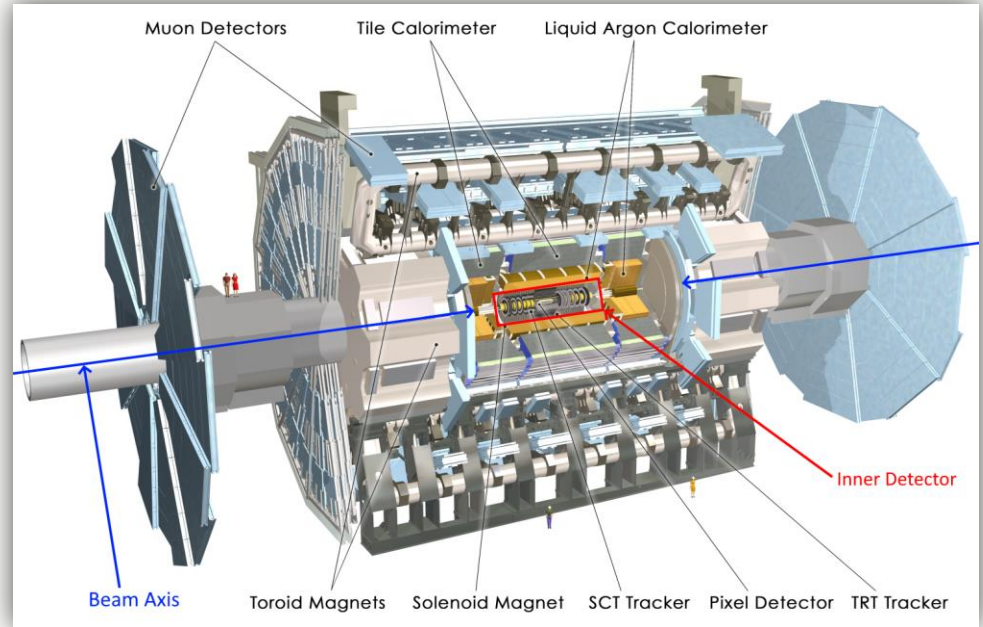
- HL-LHC will have **5 to 7 times the luminosity** of the current LHC
- Increased radiation and data collection rates
- **Replacement** of multiple **detectors** needed



<https://cds.cern.ch/record/1708847> (09. 08. 23)

# THE ATLAS DETECTOR

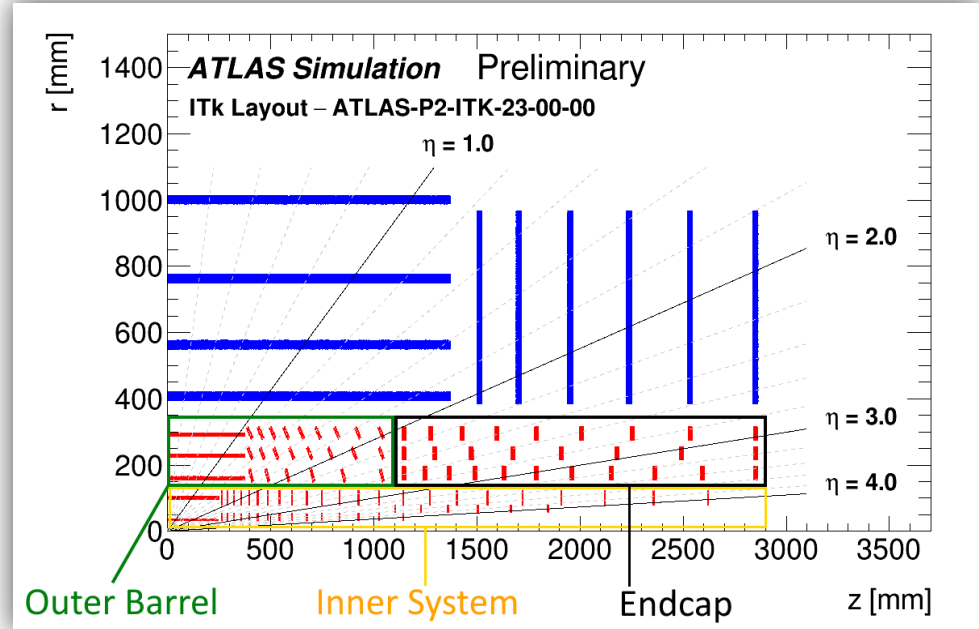
- Largest multi purpose detector in the LHC
- ATLAS will be upgraded for use in the HL-LHC
- Replacement of current Inner Detector with **new Inner Tracker detector**



<https://cds.cern.ch/record/1095924> (25.07.23), modified

## NEW ITK DETECTOR

- All-silicon particle detector
- **Improved** radiation tolerance, data collection rates, resolution and pseudorapidity coverage
- Assembly and **quality control** of **Local Supports** for the Outer Barrel at the University of Bonn



<https://atlas.web.cern.ch/Atlas/GROUPS/PHYSICS/PLOTS/ITK-2020-002/> (24.07.23), modified



## ITK LOCAL SUPPORTS

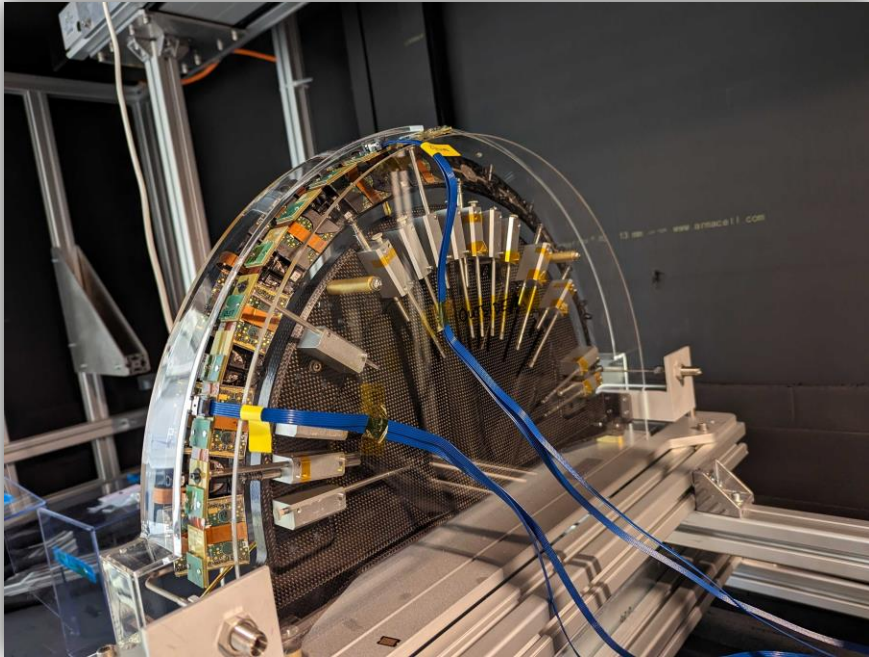
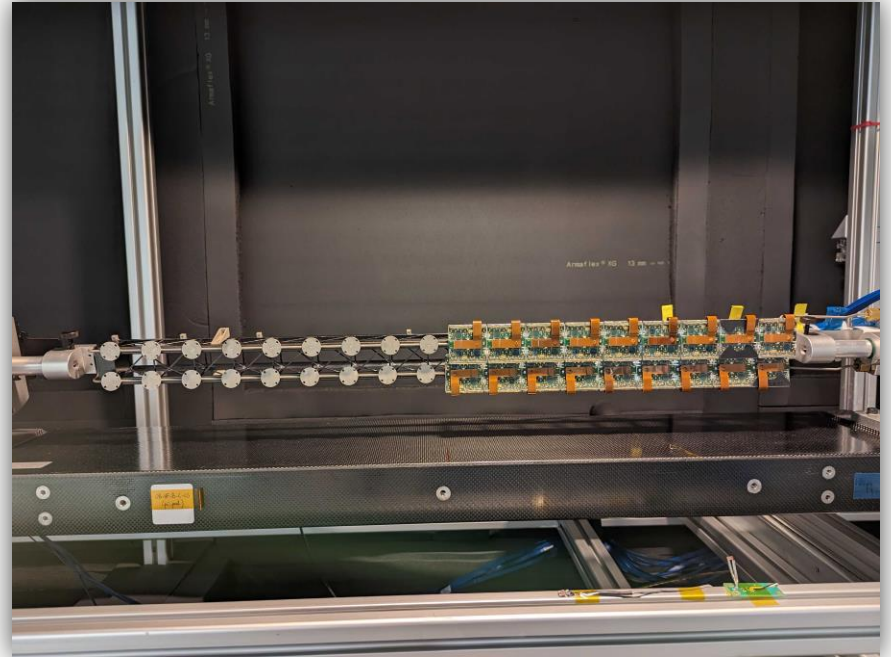


Image credit: Alexandra Wald





Approx. 400 W of cooling power needed

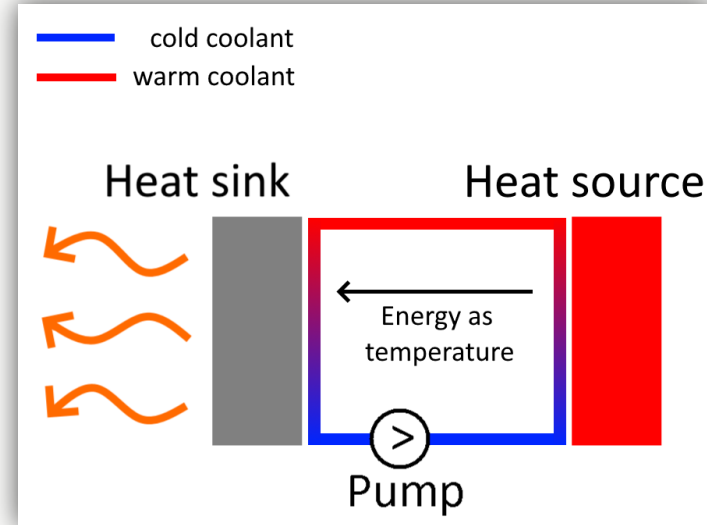
Image credit: Alexandra Wald



# Cooling systems

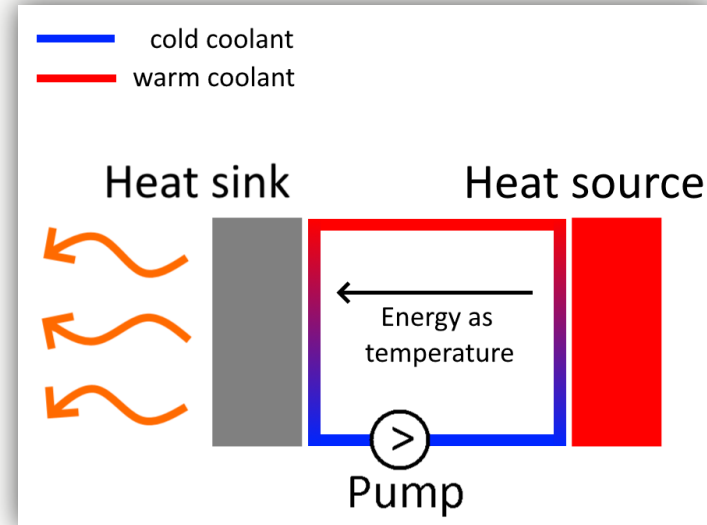
## SINGLE-PHASE COOLING

- Fluid or gaseous coolant
- **Energy** from heat source **increases the coolant temperature**
- Coolant is cooled down in heat sink
- **Problem** for detectors:  $ENC \propto T^2$



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### Advantage

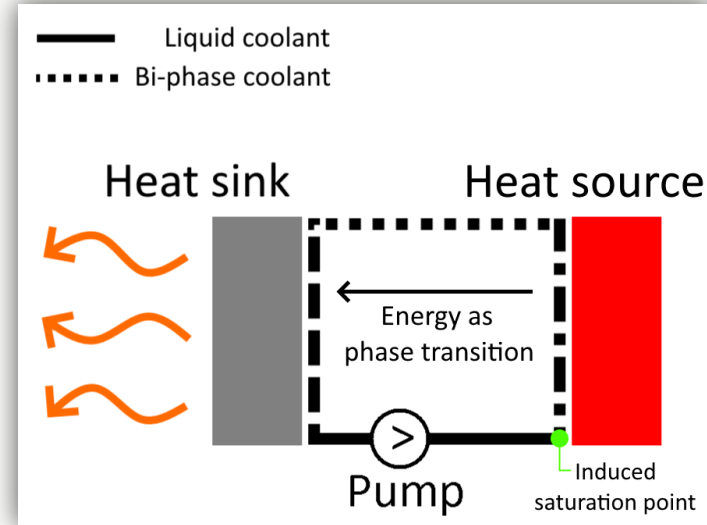
Very simple and cheap

### Disadvantage

Coolant temperature rises along heat source

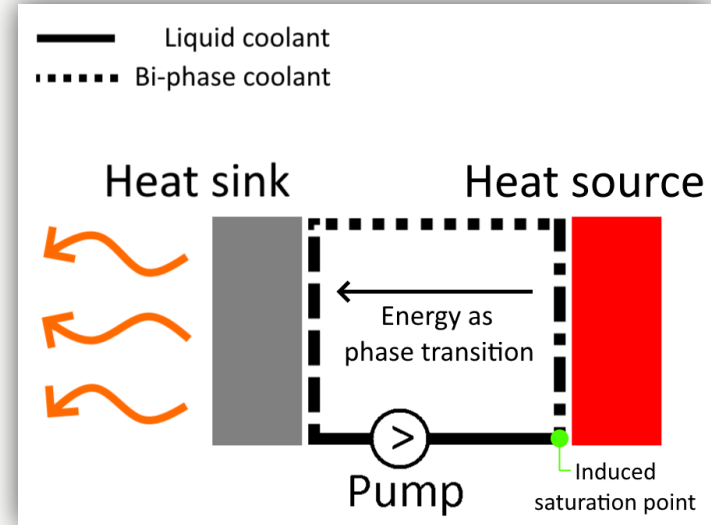
## BI-PHASE COOLING

- **Energy** from heat source causes coolant **phase transition**
- Coolant needs to be at **saturation point**
- **Risk of dry-out**



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### Advantage

Constant coolant temperature along heat source

### Disadvantage

Difficult control of coolant temperature



- Accumulator holds bi-phase coolant
- In bi-phase: **const. temperature = const. pressure**
- Regulate **temperature of accumulator** thus pressure
- Negligible pressure drop along cooling pipe between accumulator and heat source
- >Control of coolant **temperature at heat source**

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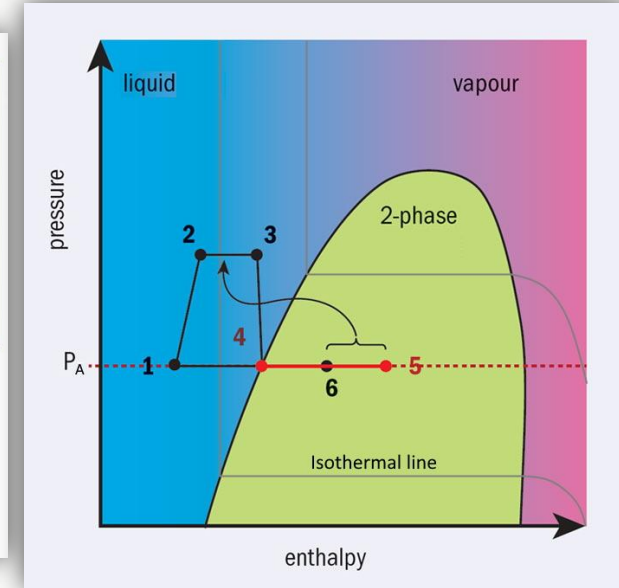
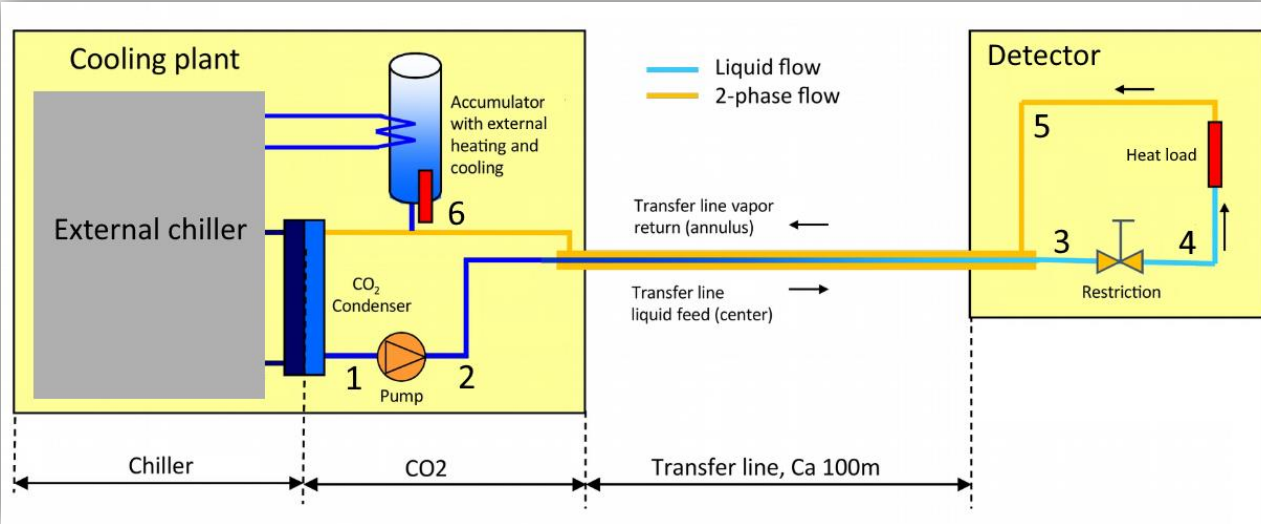
### Advantage

'Remote control' of temperature in detector

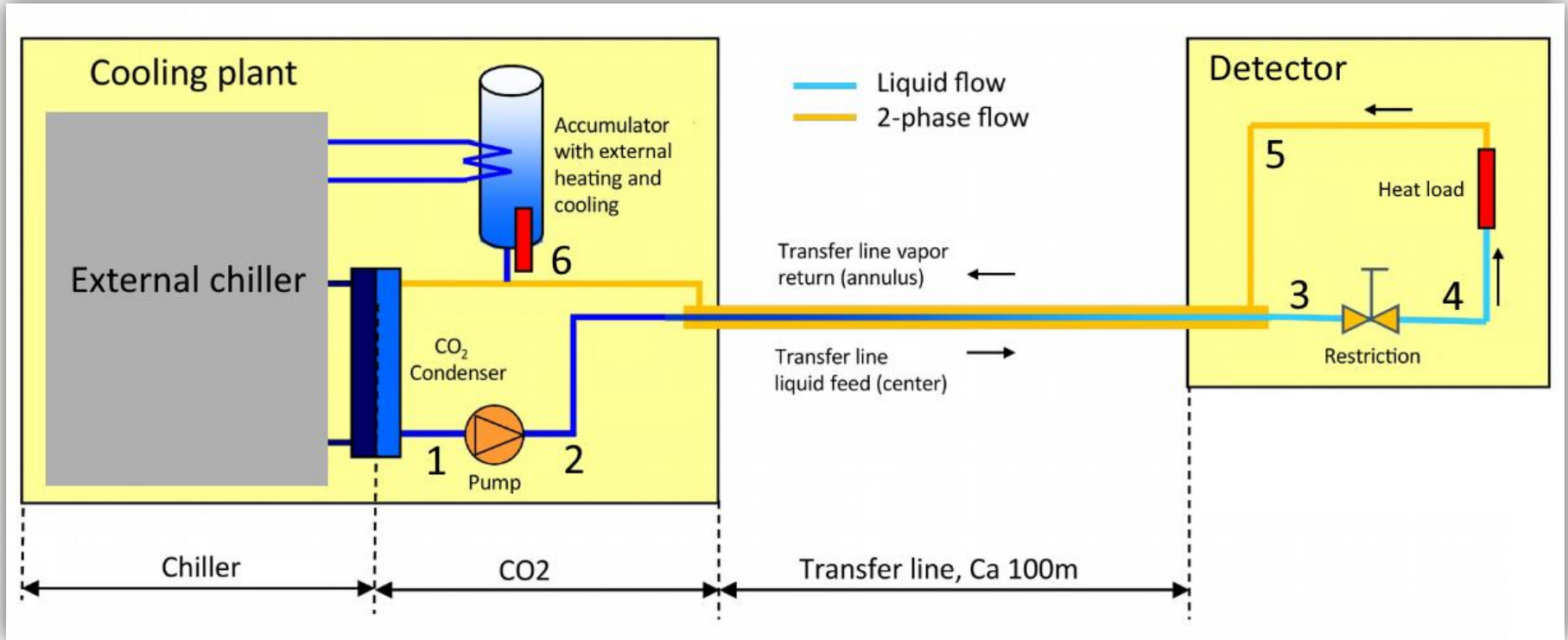
### Disadvantage

Complex and difficult to maintain

# 2PAQL IN DETAIL

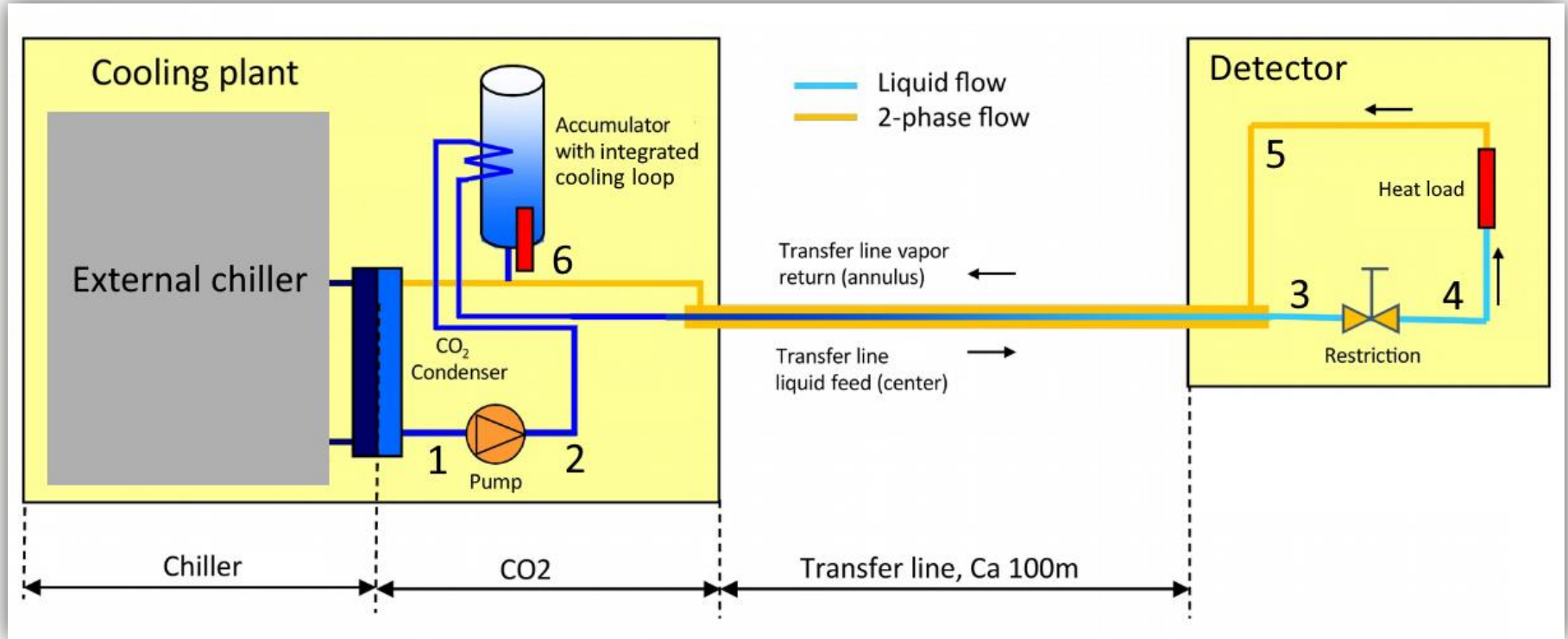


# FROM 2PACL TO INTEGRATED-2PACL



B. Verlaet u. a., *The ATLASIBL CO<sub>2</sub> cooling system*, modified

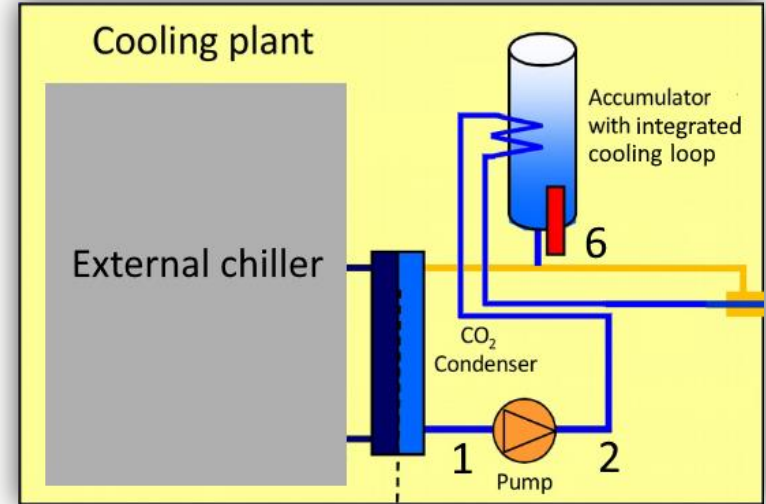
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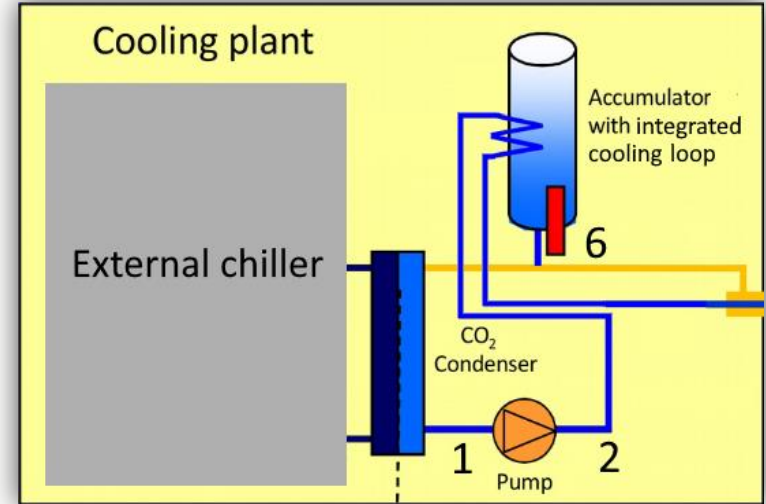


- Accumulator is cooled by the coolant itself
- Coolant temperature in detector only controlled by a heater in the accumulator
- Reduced efficiency and **cooling power limited by chiller**
- When max. **cooling capacity is exceeded** system **heats up** to new stable temperature



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## Advantage

Simpler and cheaper, decreased risk of dry-out

## Disadvantage

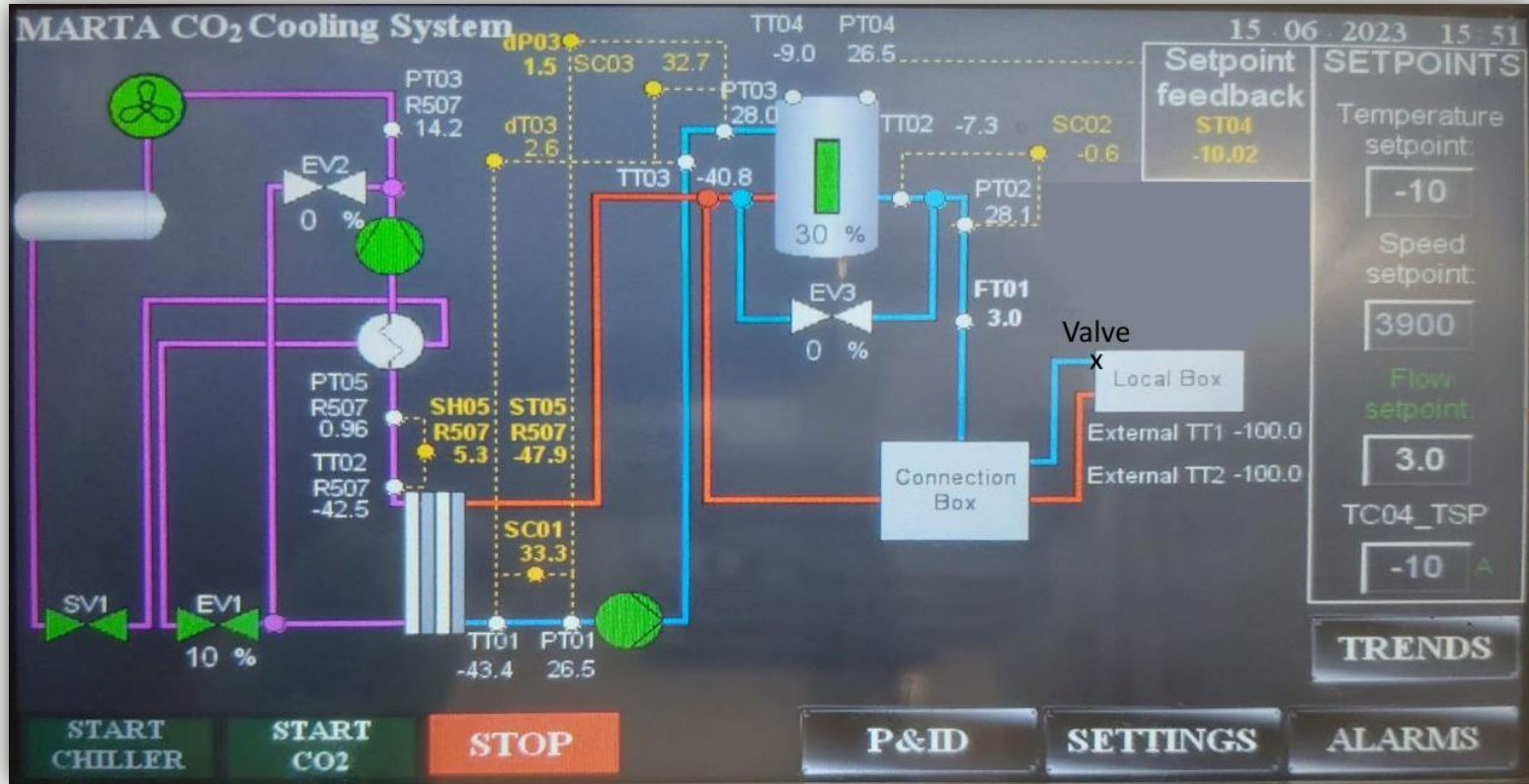
Limited cooling power and efficiency

# Characterization of MARTA

## Important parameters:

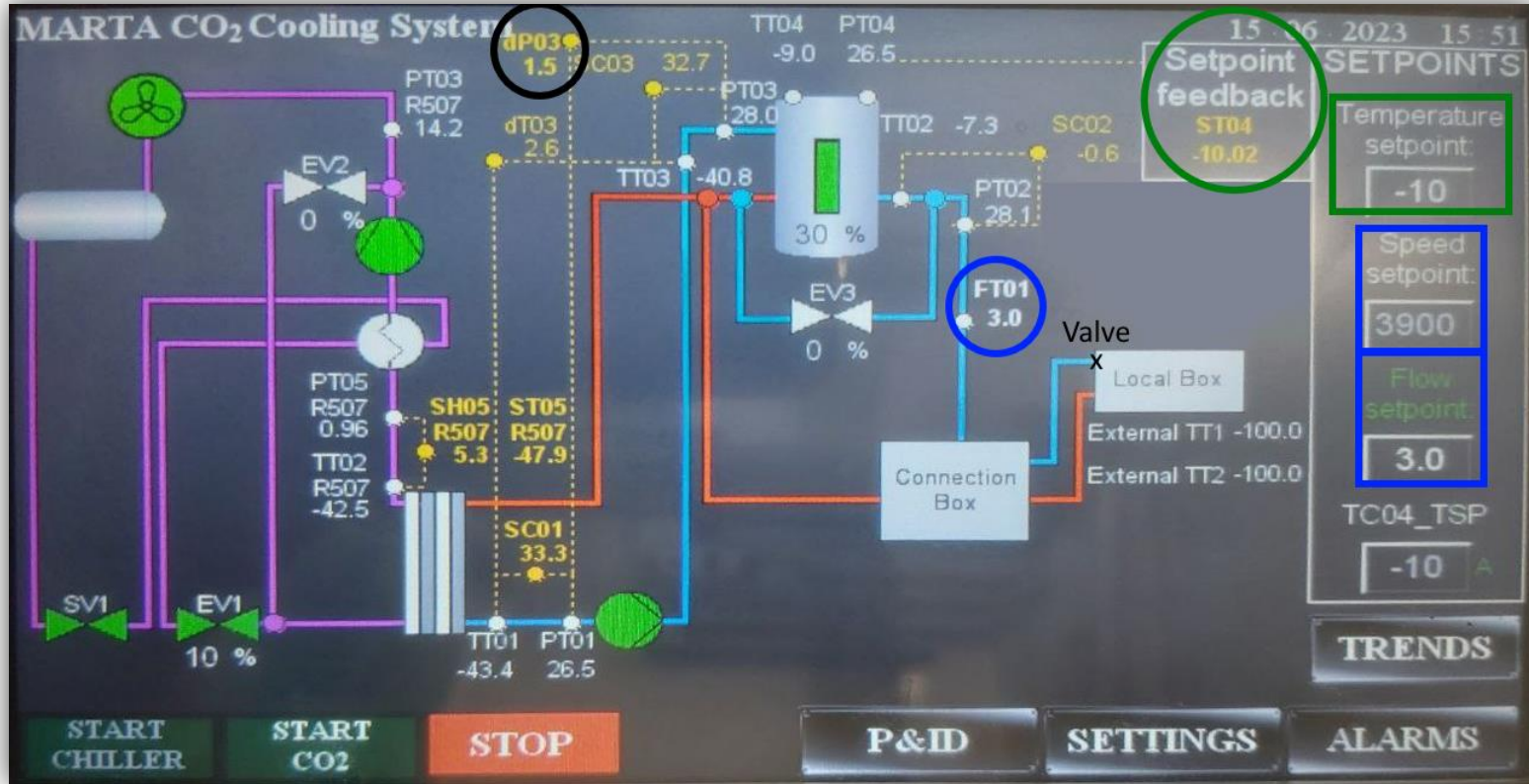
- Temperature set-point  $T_{\text{set}}$
- Temperature feedback  $T_{\text{fbk}}$
- CO<sub>2</sub>-flow rate  $q_{\text{CO}_2}$
- CO<sub>2</sub>-pump speed  $f_{\text{pump}}$
- Pump delta pressure  $dP_{\text{pump}}$
- Only CO<sub>2</sub>-**flow rate or -pump speed** can be controlled at the same time
- $dP_{\text{pump}}$  **must be** between 1 – 6 bar

# HOW TO OPERATE MARTA

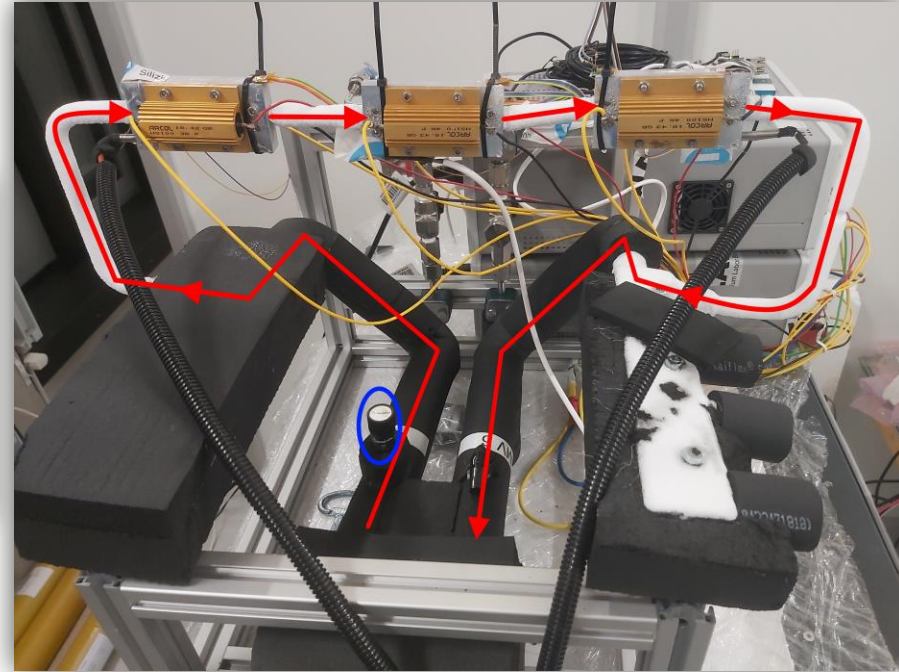
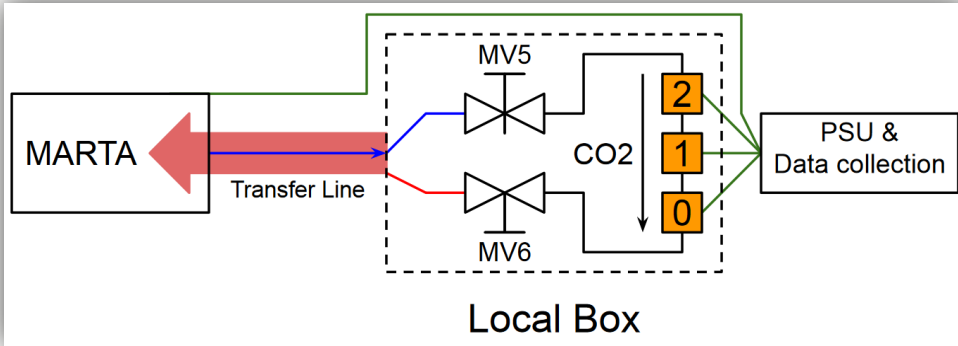




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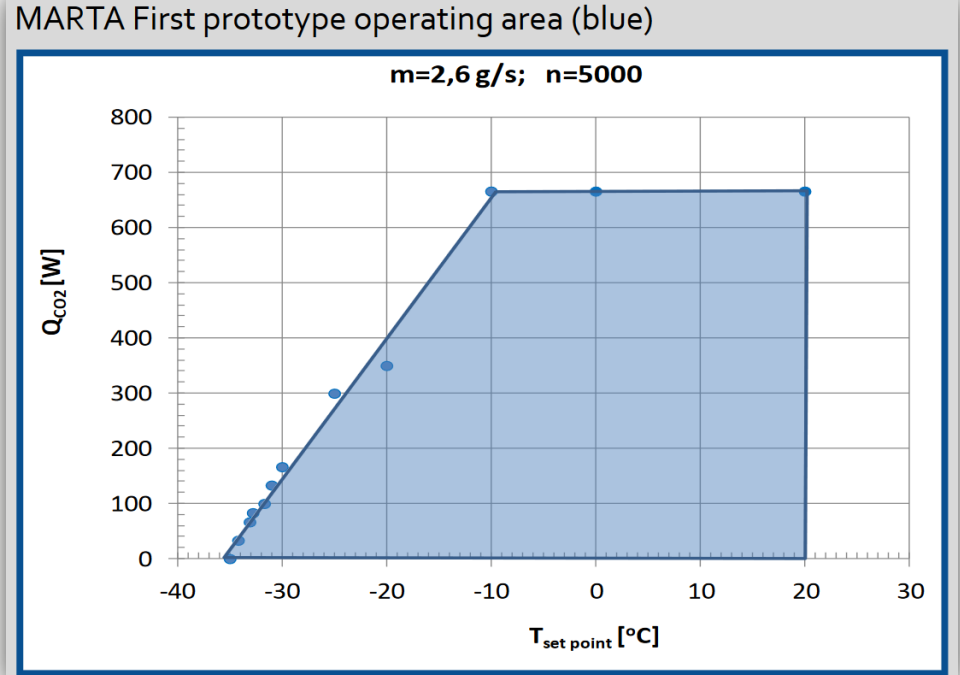


# SETUP FOR MEASURING THE COOLING POWER



## COOLING POWER OF MARTA

- For every heat load there is a **minimal stable  $T_{\text{set}}$**
- This creates a **stable operating area**
- **Below** this temperature the system simply **heats up** to the operating area

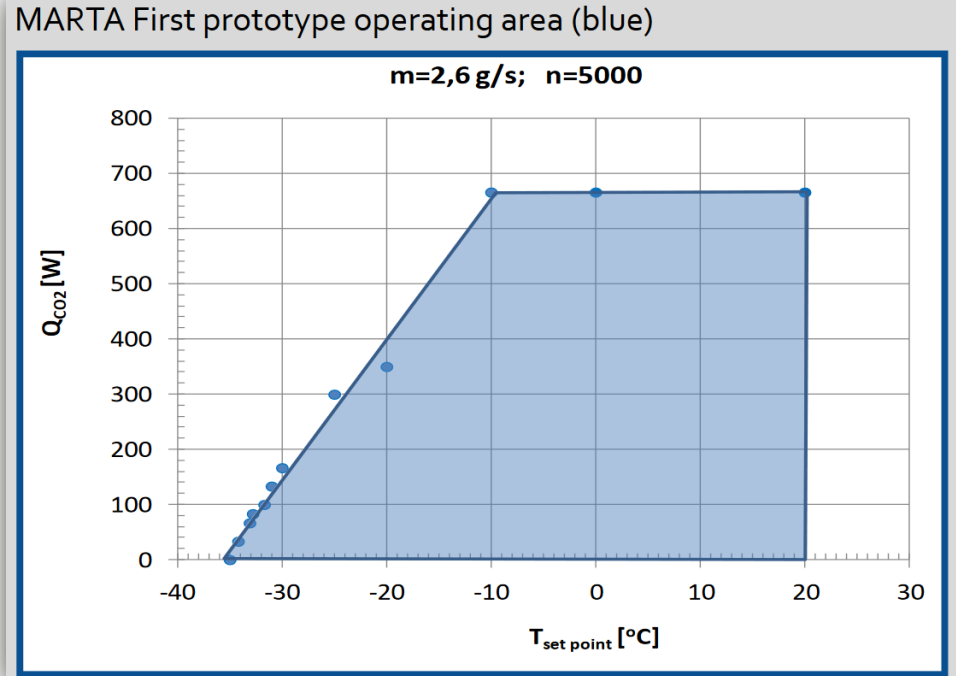


[https://indico.cern.ch/event/590227/contributions/2614149/attachments/1487980/2311754/MARTA\\_-\\_Monoblock\\_Approach\\_for\\_a\\_Refrigeration\\_Technical\\_Application.pdf](https://indico.cern.ch/event/590227/contributions/2614149/attachments/1487980/2311754/MARTA_-_Monoblock_Approach_for_a_Refrigeration_Technical_Application.pdf) (22.07.23)

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E.g. at 600 W heat load and  $T_{\text{set}} = -30\text{ °C}$   
 $T_{\text{fbk}}$  will simply rise to  $-12\text{ °C}$

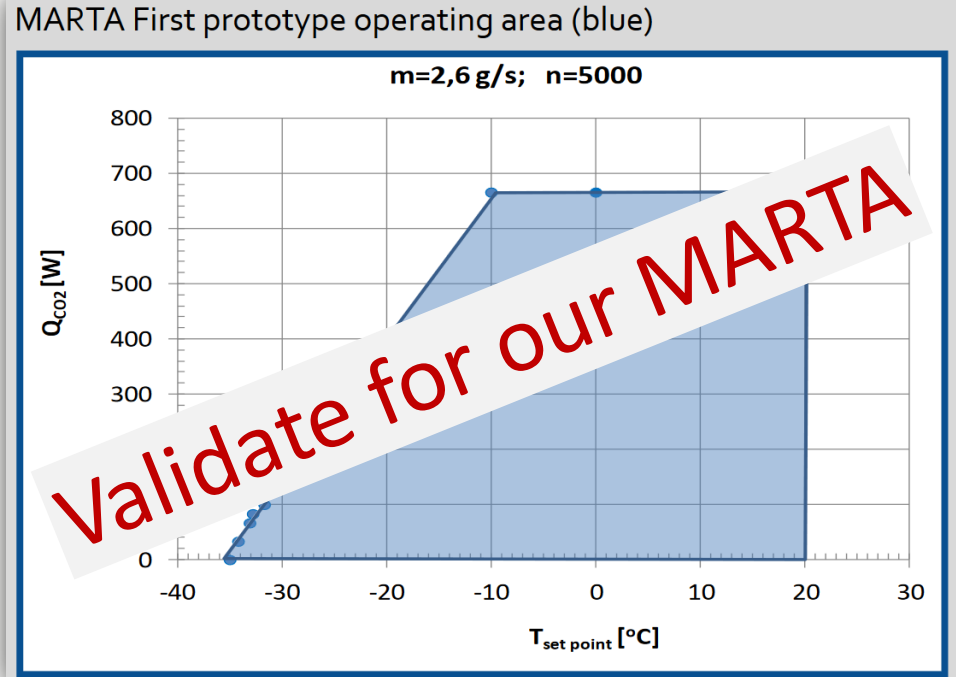


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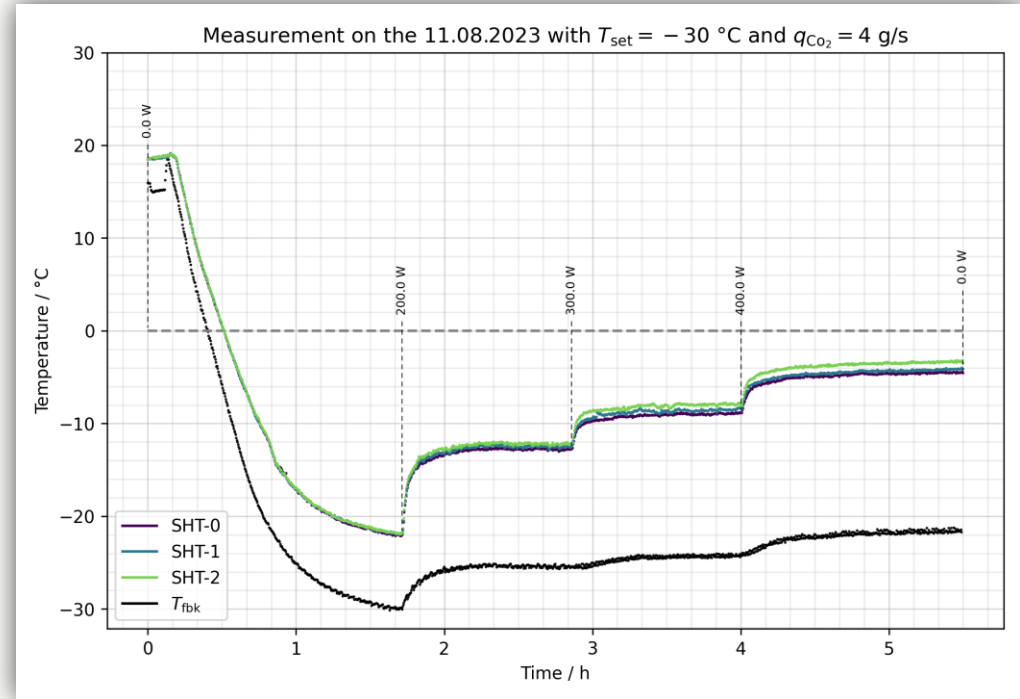


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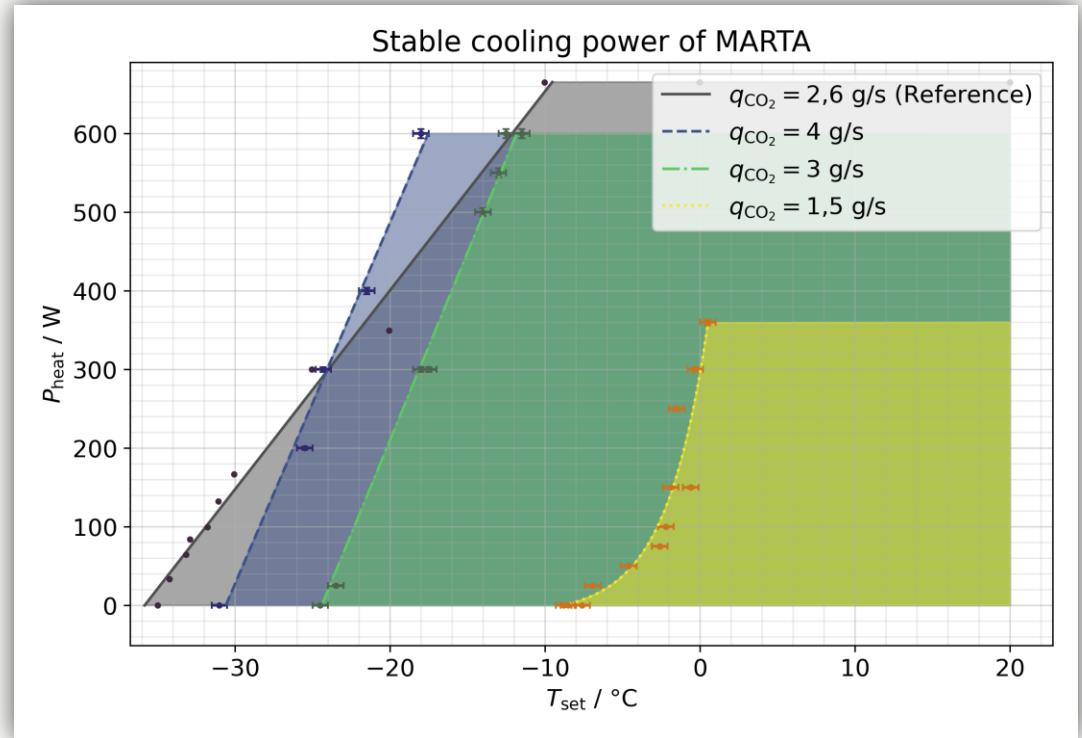


## EXAMPLE MEASUREMENT

- System cools down with no heat load
- **Heat load is applied** until heat-up
- **Record  $T_{fbk}$**  when thermal equilibrium is achieved
- Increase heat load, repeat

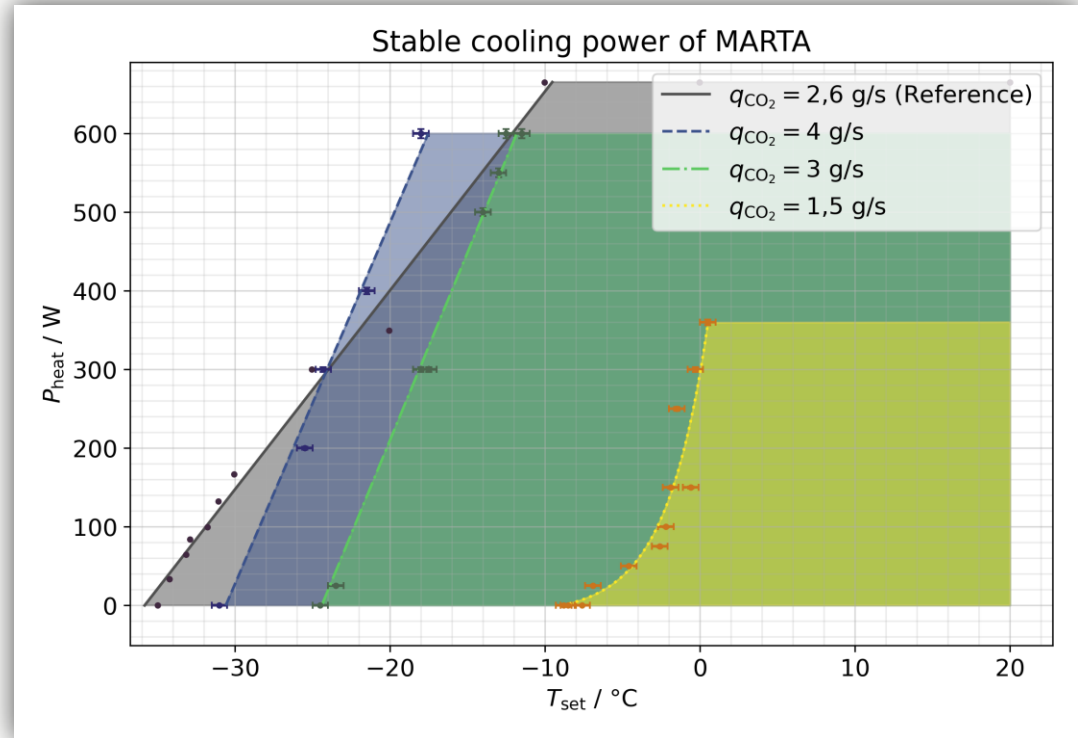


# RESULTS FOR THE ITK-QC



## RESULTS FOR THE ITK-QC

- Cooling power lower than anticipated
- At 400 W  $\text{CO}_2$  temperature of below  $-15\text{ °C}$  possible
- Expected max. pixel module temperature below  $10\text{ °C}$



## SUMMARY AND OUTLOOK

- Understanding the concept and operation of the cooling system in MARTA
- **Characterization of MARTA**
- Evaluation of cooling capabilities for ITk-QC
- Outlook:
  - Implementation of MARTA for the ITk-QC
  - **Further investigation of MARTA** edge case characteristics

*Technical Design Report for the ATLAS Inner Tracker Strip Detector, Techn. Ber., CERN, 2017, url: <https://cds.cern.ch/record/2257755>*

*P. Barroca, Modelling CO2 cooling of the ATLAS ITk Pixel Detector, Diss., 2019, url: <https://cds.cern.ch/record/2703341>*

*B. Verlaat, M. Van Beuzekom und A. Van Lysebetten, CO2 cooling for HEP experiments, 2008, url: <https://cds.cern.ch/record/1158652>*

Conversations with M. Hamer, F. Hinterkeuser, K. Padeken

THANK YOU!

Any questions?

## Detailed differences between ITk and ID

- ITk is just better!
- Also pseudorapidity increase from 2.5 to 4
- ITk needs a lot more cooling

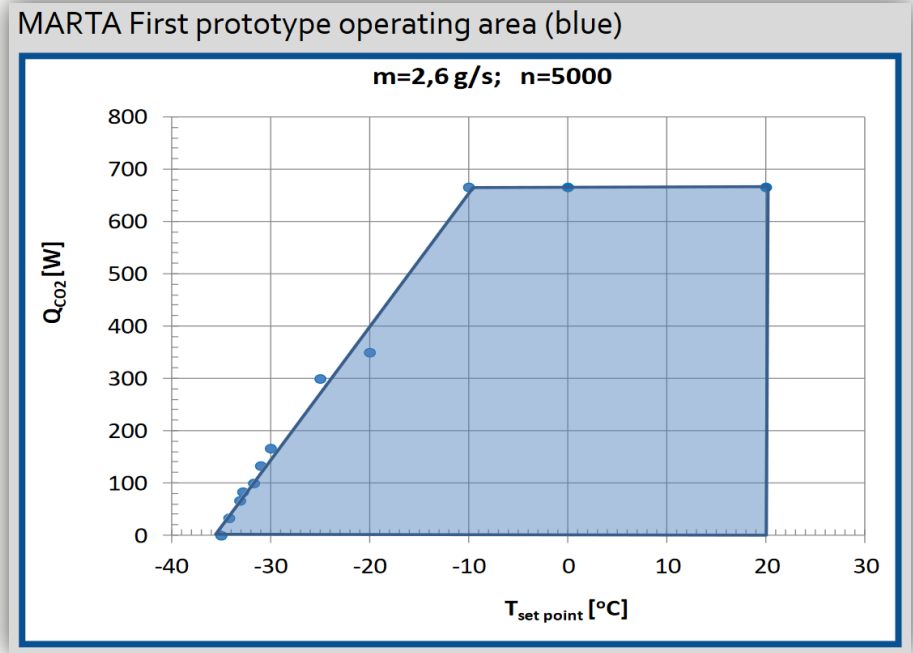
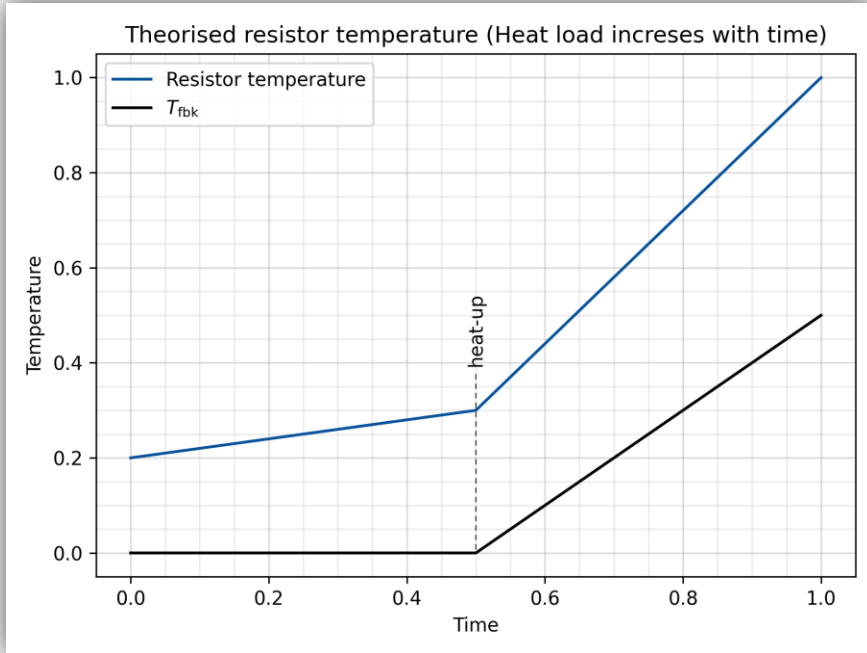
	ATLAS Pixel + IBL	ITk Pixel
Modules	2000	8500
Pixel Size	$50 \times 400 \mu\text{m}^2$ or $50 \times 250 \mu\text{m}^2$	$50 \times 50 \mu\text{m}^2$
Readout channels	80 million	5 billion
Active area	$1.7 \text{ m}^2$	$14 \text{ m}^2$
TID	2.5 MGy	10 MGy
Fluence	$10^{15} \text{ n}_{\text{eq}}/\text{cm}$	$1.4^{16} \text{ n}_{\text{eq}}/\text{cm}$
Trigger rate	100 kHz	1 MHz
FE data rate	160 Mb s	5.12 Gb s
Powering	parallel	serial
Cooling budget	15 kW	100 kW



## Methods for finding the max. cooling capacity

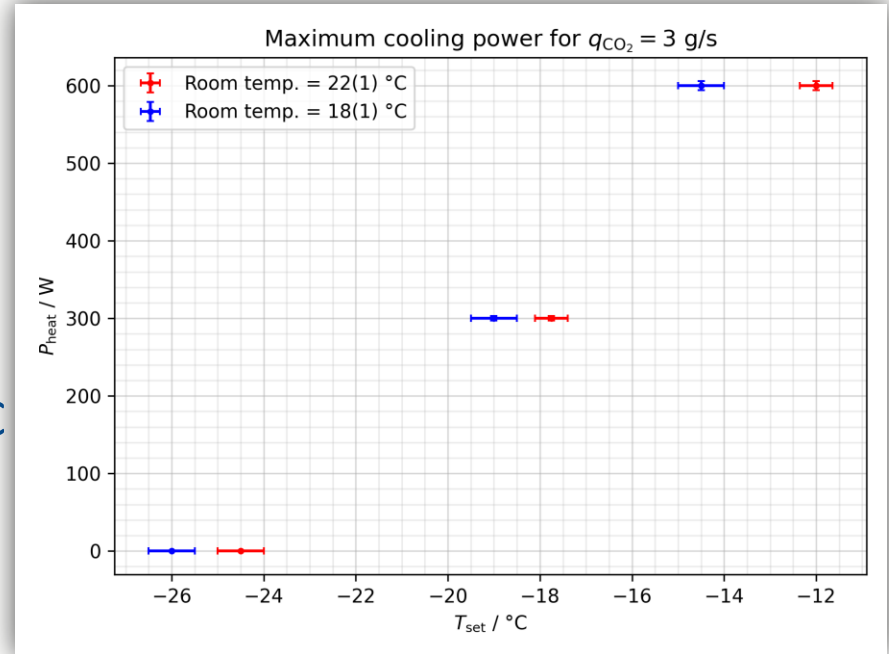
Method	Resistor Temperature for the start of heat-up	$T_{fbk}$ for the start of heat-up	Constant heat-up
<b>Description</b>	Find sudden increase in resistor temperature	Increase heat load until heat-up is observed	Start system in heat-up, measure $T_{fbk}$ for selected heat loads
<b>Evaluation</b>	Temperature measurement too inaccurate	Takes a long time to stepwise increase heat load and wait for heat-up	Quickly measure along the line of max. cooling power

# Methods for finding the max. cooling capacity



# Does room temperature effect cooling power?

Lowering of room temperature by 4(1) °C  
 only improved cooling capacity by 1.8(4) °C



## Why is the $q_{\text{CO}_2} = 1.5 \text{ g/s}$ operating range limited?

- **Insufficient thermal connection** between the resistors and the cooling pipe at **higher temperature**
- The heat transfer suddenly collapses
- **Resistor quickly heats up** out of safe operating temperature
- No safe measurement possible

